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Citation: Wang, Ke, Qu, Yuwei, Yuan, Jinhui, Qiu, Shi, Zhou, Xian, Yan, Binbin, Wu, Qiang, Liu, Bin, Wang, Kuiru, Sang, Xinzhu and Yu, Chongxiu (2021) Ultra-short polarization beam splitter based on dual-core photonic crystal fiber with surface plasmon resonance effect. Optical Engineering, 60 (07). 076104. ISSN 0091-3286

Published by: SPIE

URL: <https://doi.org/10.1117/1.oe.60.7.076104>  
<<https://doi.org/10.1117/1.oe.60.7.076104>>

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# An ultra-short polarization beam splitter based on dual-core photonic crystal fiber with surface plasmon resonance effect

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**Abstract.** In this paper, an ultra-short polarization beam splitter (PBS) based on dual-core photonic crystal fiber (DC-PCF) with surface plasmon resonance (SPR) effect is proposed. The finite element method is used to investigate the coupling characteristics between the core mode and surface plasmon polariton (SPP) mode. The influences of the PCF structure parameters on the coupling length ( $CL$ ) and coupling length ratio ( $CLR$ ) are also investigated. The normalized output powers of the x-polarization and y-polarization are calculated, and the optimized PBS achieves an ultra-short length of 62.5  $\mu\text{m}$ . The splitting bandwidth of 110 nm (1.51~1.61  $\mu\text{m}$ ) is achieved when the extinction ratio ( $ER$ ) is less than -20 dB. The minimum  $ER$  reaches -71 dB at the wavelength of 1.55  $\mu\text{m}$ . The proposed PBS has an important application in the high-speed optical communication system.

**Keywords:** polarization beam splitter, photonic crystal fiber, surface plasmon resonance, extinction ratio.

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## 1. Introduction

With the rapid development of the communication system, the polarization characteristics of optics have attracted great attention. Because the polarization beam splitter (PBS) can split a beam of light into two polarized beams 1, it has widespread applications in optical communication and sensing systems. The larger refractive index difference between the two polarization beams is the key to achieve the PBS with shorter length and wider bandwidth. However, it is difficult to obtain the larger refractive index difference for the traditional dual-core optical fibers because of their structural symmetry and low birefringence 2. Compared with the traditional optical fibers, photonic crystal fiber (PCF) has unique optical characteristics, such as endlessly single-mode 5,6, high birefringence 7, large mode field area 10, controllable dispersion 11, and high nonlinearity 12. Thus, the PCF can be applied for different devices. For example, the PCF-based PBS with shorter length and wider bandwidth could be -achieved.

In recent years, some researchers designed different kinds of PBS based on the dual-core PCF (DC-PCF) through breaking the structural symmetry of the DC-PCF, which can be achieved by changing the arrangement of the air holes in the cladding region 19 or introducing the elliptical air holes 19. Moreover, other materials can also be used for replacing the silica substrate and the metal materials can be used for coating or filling the air holes. In 2015, Xu *et al.* reported a DC-PCF PBS with an elliptical hole, which is filled with a kind of low refractive index material. The length and bandwidth of the reported PBS are 401  $\mu\text{m}$  and 140 nm 22. In

2016, Wang *et al.* designed a DC-PCF PBS filled with the liquid crystal in the air hole, achieving the PBS length of 890.5  $\mu\text{m}$  and bandwidth of 150 nm <sup>23</sup>. In 2017, Wang *et al.* proposed a DC-PCF PBS with the magnetic fluid added in the air hole, where the PBS length and bandwidth are 5.1 mm and 189 nm <sup>24</sup>. In 2018, Wang *et al.* reported a rectangular-hexagonal structure DC-PCF PBS with two elliptical holes in the core region, along with the PBS length of 93.3  $\mu\text{m}$  and bandwidth of 40 nm <sup>25</sup>. In 2019, Xu *et al.* demonstrated a DC-PCF PBS filled with titanium and low refractive index liquid, where the PBS length and bandwidth are 83.9  $\mu\text{m}$  and 32.1 nm <sup>26</sup>. In 2020, Qu *et al.* investigated a gold-coated silicon DC-PCF PBS, where the PBS length and mid-infrared bandwidth are 192  $\mu\text{m}$  and 830 nm <sup>27</sup>.

In this paper, we propose an ultra-short PBS based on the gold-filled DC-PCF. The two cores of the DC-PCF are composed by the three elliptical air holes in the horizontal axis. Two elliptical gold wires are filled in longitudinal axis to induce the surface plasmon resonance (SPR) effect. The PBS can achieve an ultra-short length of 62.5  $\mu\text{m}$  and a bandwidth of 110 nm. The proposed DC-PCF PBS has an important application in the high-speed optical communication system.

## 2. Design of the DC-PCF PBS and theory

The cross-section of the proposed DC-PCF PBS is shown in Fig. 1. The diameter of all circular air holes arranged in the triangular array is  $d$ , and the hole-to-hole pitch is  $A_1$ . In addition, the three layers of air holes are arranged in a rectangular array in the horizontal direction, and the hole-to-hole pitch is  $A_2$ . The air hole in the most center is replaced with an elliptical hole, whose minor and major axes are denoted by  $d_{x1}$  and  $d_{y1}$ , respectively. And the two air holes are missing on the left and right sides of the central elliptical air hole to form the cores A and B, respectively. The air holes on the upper and lower sides of the central elliptical hole are filled by the two elliptical gold wires, whose minor and major axes are denoted by  $d_{y2}$  and  $d_{x2}$ , respectively. Compared with other metal materials, the gold material has stable chemical property, good biomolecular compatibility, and strong corrosion resistance. The left side of the core A and right side of the core B are replaced by the two large elliptical air holes, whose minor and major axes are denoted by  $d_{x3}$  and  $d_{y3}$ , respectively.

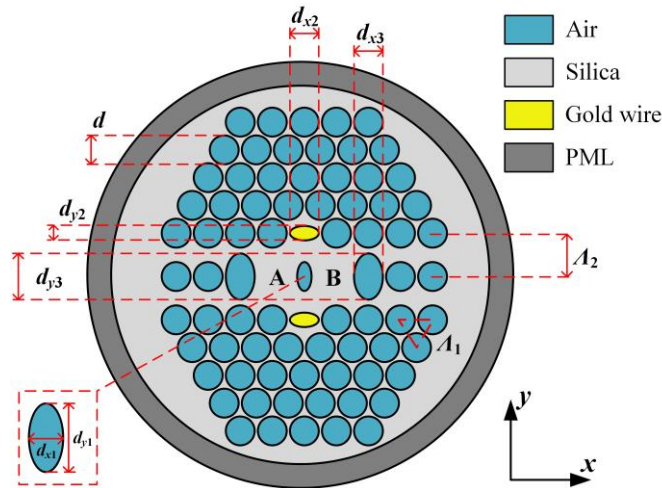


Fig. 1. The cross-section of the proposed DC-PCF PBS.

The background material is the pure silica. The perfect matching layer (PML) of the proposed DC-PCF is set at the outermost layer to absorb the radiation energy <sup>28</sup>. The inner diameter and thickness of the PML are 6  $\mu\text{m}$  and 1.2  $\mu\text{m}$ , respectively. The material of the PML

is highly doped silica, and the corresponding refractive index is  $n_{\text{silica}}+0.03$ . The material dispersions of the silica and doped silica can be described by the Sellmeier equation [29, 30]. The dielectric constant of the gold material can be described by the Drude-Lorentz [31]

$$\varepsilon_m = \varepsilon_\infty - \frac{\omega_D^2}{\omega(\omega + j\gamma_D)} - \frac{\Delta\varepsilon \cdot \Omega_L^2}{(\omega^2 - \Omega_L^2) - j\Gamma_L\omega}, \quad (1)$$

where  $\varepsilon_m$  represents the dielectric constant of gold,  $\varepsilon_\infty = 5.9673$  is the high frequency dielectric constant,  $\Delta\varepsilon = 1.09$  is the wave vector,  $\omega$  is the angular frequency of the light, and  $\omega_D$  and  $\gamma_D$  are the plasma frequency and Damping frequency, respectively. Here,  $\omega_D/2\pi = 2113.6$  THz, and  $\gamma_D/2\pi = 15.92$  THz.  $\Omega_L$  and  $\Gamma_L$  are the frequency and spectral width of the Lorentz oscillation, respectively.  $\Omega_L/2\pi = 650.07$  THz, and  $\Gamma_L/2\pi = 104.86$  THz.

The coupling length ( $CL$ ) of the DC-PCF, where the light power is completely transferred from one core to the other one, can be calculated by [32]

$$CL_{x,y} = \frac{\lambda}{2(n_{x,y}^{\text{even}} - n_{x,y}^{\text{odd}})}, \quad (2)$$

where the  $CL_{x,y}$  is the  $CL$  of the  $x$ -pol and  $y$ -pol,  $\lambda$  is the wavelength of the incident light, and  $n$  is the effective refractive indices of the even and odd modes. In order to achieve the complete beam splitting, the  $CL$  of the two polarization states needs to satisfy the condition that  $mCL_x = nCL_y = L$  ( $m$  and  $n$  are the positive integers and  $L$  is the length of the PBS), and the coupling length ratio ( $CLR$ ) can be calculated by

$$CLR = \frac{CL_y}{CL_x}, \quad (3)$$

When the  $CLR$  reaches 2 or 0.5, the splitting length is the optimum value. The transmission loss of the ultra-short PBS is also negligible. Therefore, when the input power  $P_{\text{in}}$  is determined, the normalized output power  $P_{\text{out}}$  can be calculated by [33]

$$P_{\text{out}}^{x,y} = P_{\text{in}}^{x,y} \cos^2\left(\frac{\pi L}{2CL_{x,y}}\right), \quad (4)$$

The performance of the PBS can be described by the extinction ratio ( $ER$ ) as following [34]

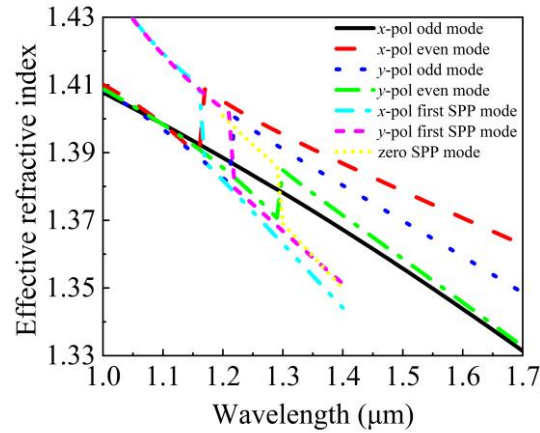
$$ER = 10 \cdot \lg\left(\frac{P_{\text{out}}^y}{P_{\text{out}}^x}\right), \quad (5)$$

when the  $ER$  is larger than 20 dB, the propagated light could be completely split, so the  $ER$  can determine the bandwidth of the PBS.

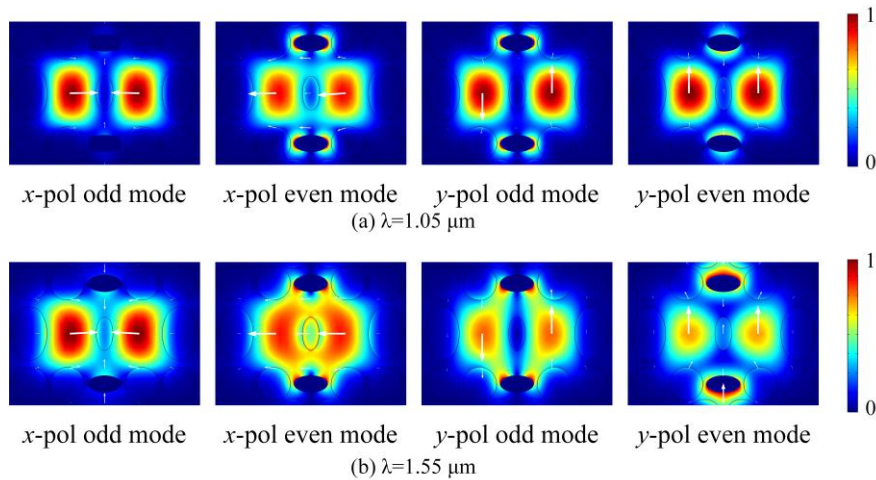
### 3. Simulation results and discussion

The finite element method (FEM) is adopted to simulate the proposed DC-PCF PBS. Fig. 2 shows the calculated effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and even modes,  $x$ -pol and  $y$ -pol first SPP modes, and zero SPP mode. From Fig. 2, the  $x$ -pol even mode and  $x$ -pol first SPP mode have a resonance point at wavelength 1.17  $\mu\text{m}$ , the  $y$ -pol odd mode and  $y$ -pol first SPP mode have a resonance point at wavelength 1.22  $\mu\text{m}$ , and the  $y$ -pol

even mode and zero SPP mode have a resonance point at wavelength 1.3  $\mu\text{m}$ , while there is no resonance point between the  $x$ -pol odd mode and SPP mode. According to the coupling mode theory 35, the  $x$ -pol even,  $y$ -pol odd, and  $y$ -pol even modes are completely coupled with the  $x$ -pol first SPP,  $y$ -pol first SPP, and zero SPP modes, respectively. In order to further verify the above conclusions, the mode field distributions of the  $x$ -pol and  $y$ -pol even and odd modes at wavelengths 1.05  $\mu\text{m}$  and 1.55  $\mu\text{m}$  are shown in Figs. 3(a) and 3(b), respectively. From Fig. 3(a), the mode field energies of the  $x$ -pol and  $y$ -pol odd and even modes do not occur to change at wavelength 1.05  $\mu\text{m}$ , which indicate that before wavelength 1.05  $\mu\text{m}$ , there are no mode coupling between the considered modes and SPP modes. From Fig. 3(b), the mode field energy of the  $x$ -pol odd mode does not occur to change, and the mode field energies of the  $x$ -pol even,  $y$ -pol odd, and  $y$ -pol even modes occur to transfer. It indicates that the  $x$ -pol even,  $y$ -pol odd, and  $y$ -pol even modes occur to couple with the  $x$ -pol first SPP mode,  $y$ -pol first SPP mode, and zero SPP mode, respectively, after 1.55  $\mu\text{m}$ . Because the coupling strengths based on the SPR effect for different modes are different, the effective refractive index differences between the  $x$ -pol and  $y$ -pol modes are increased, and the DC-PCF PBS could be achieved due to the enhanced birefringence.

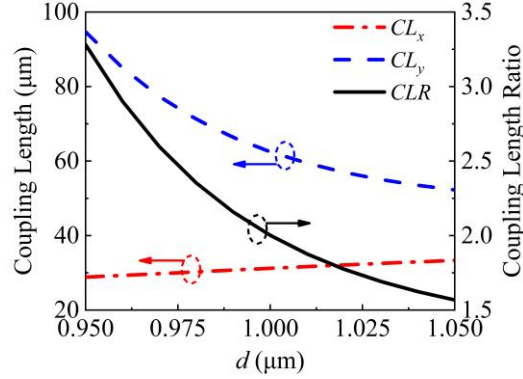


**Fig. 2.** The effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and even modes,  $x$ -pol and  $y$ -pol first SPP modes, and zero SPP mode calculated as functions of wavelength.



**Fig. 3.** The mode field distributions of the  $x$ -pol odd mode,  $x$ -pol even mode,  $y$ -pol odd mode, and  $y$ -pol even mode calculated at wavelengths (a) 1.05  $\mu\text{m}$  and (b) 1.55  $\mu\text{m}$ .

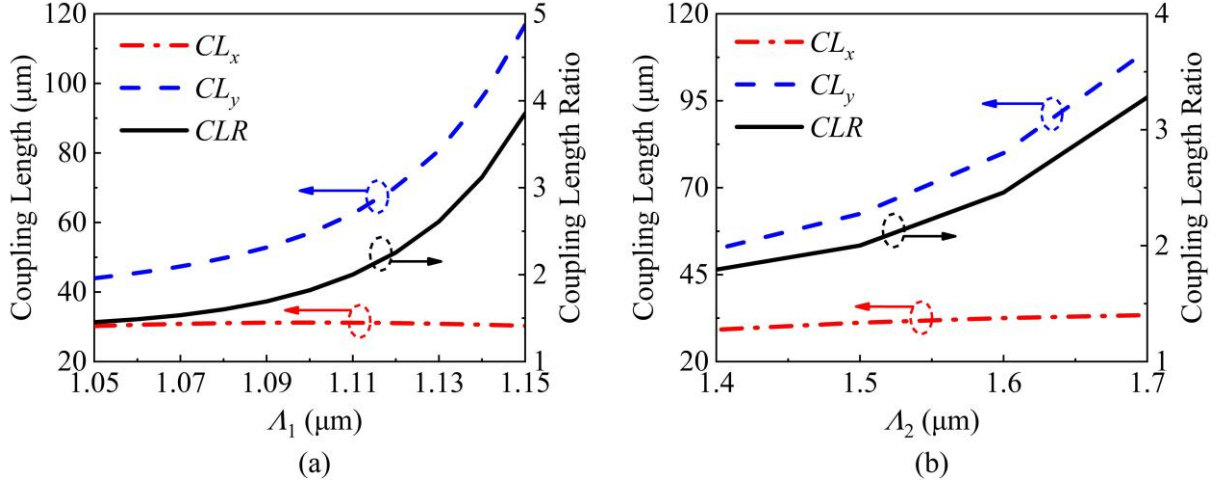
In the following, the structure parameters, including  $d$ ,  $A_1$ ,  $A_2$ ,  $d_{x1}$ ,  $d_{y1}$ ,  $d_{y2}$ ,  $d_{x2}$ ,  $d_{x3}$ , and  $d_{y3}$ , are, respectively, adjusted at wavelength  $1.55 \mu\text{m}$  to optimize the performance of the DC-PCF PBS. The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$  are shown in Fig. 4. When  $d$  changes from  $0.95$  to  $1.05 \mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and even modes decrease, but the decrease amplitude of the  $x$ -pol even mode is larger than that of the  $x$ -pol odd mode. Meanwhile, the effective refractive indices of the  $y$ -pol odd and even modes also decrease, but the decrease amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -pol odd mode. Thus, the effective refractive index differences between the  $x$ -pol odd and even modes and  $y$ -pol odd and even modes become smaller. As shown in Fig. 4, the  $CL_x$  increases from  $28$  to  $33 \mu\text{m}$ , and the  $CL_y$  decreases from  $92$  to  $52 \mu\text{m}$ . It can be deduced from Eq. (3) that the  $CLR$  decreases from  $3.2$  to  $1.5 \mu\text{m}$ . When  $d=1 \mu\text{m}$ , the  $CLR=2.048$ , which is very close to the ideal value of  $2$ .



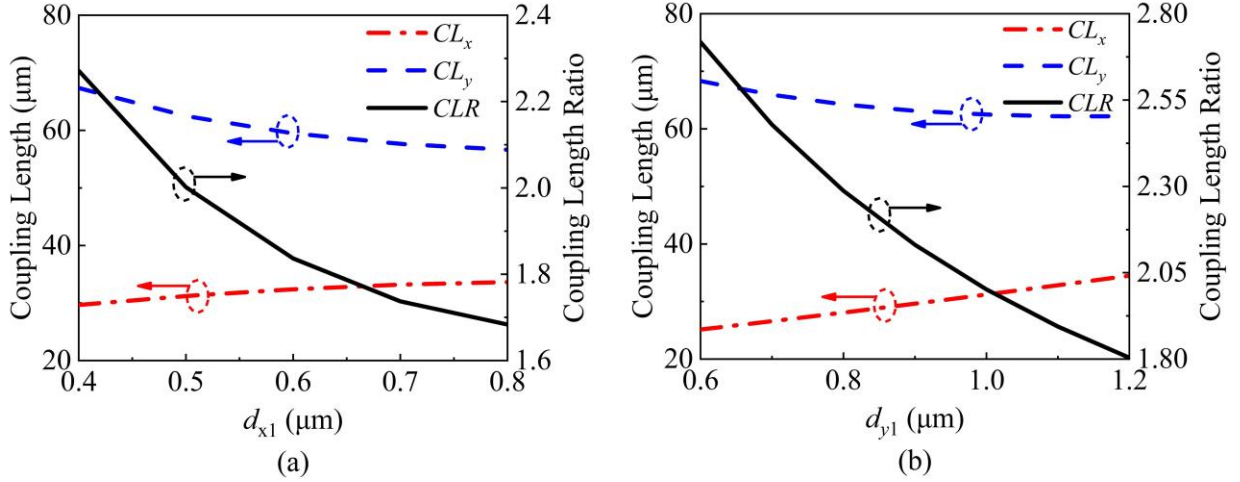
**Fig. 4.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$ .

When  $A_1$  changes from  $1.05$  to  $1.15 \mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and even modes increase, and the increase amplitude of the  $x$ -pol even mode is approximately equal to that of the  $x$ -pol odd mode. Although the effective refractive indices of the  $y$ -pol odd and even modes also increase, the increase amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -pol odd mode. Thus, the effective refractive index difference between the  $x$ -pol odd and even modes remains almost unchanged, while the effective refractive index difference between the  $y$ -pol odd and even modes becomes smaller. As shown in Fig. 5(a), the  $CL_x$  is stabilized at  $30 \mu\text{m}$ , and the  $CL_y$  increases from  $43$  to  $120 \mu\text{m}$ . According to Eq. (3), the  $CLR$  increases from  $1.4$  to  $3.8 \mu\text{m}$ . When  $A_1=1.11 \mu\text{m}$ , the  $CLR$  is very close to  $2$ . From Fig. 5(b), when  $A_2$  changes from  $1.4$  to  $1.7 \mu\text{m}$ , the  $CL_x$  increases from  $29$  to  $33 \mu\text{m}$ , the  $CL_y$  increases from  $52$  to  $109 \mu\text{m}$ , and the corresponding  $CLR$  increases from  $1.79$  to  $3.2$ . When  $A_2=1.6 \mu\text{m}$ , the  $CLR$  is very close to  $2$ .



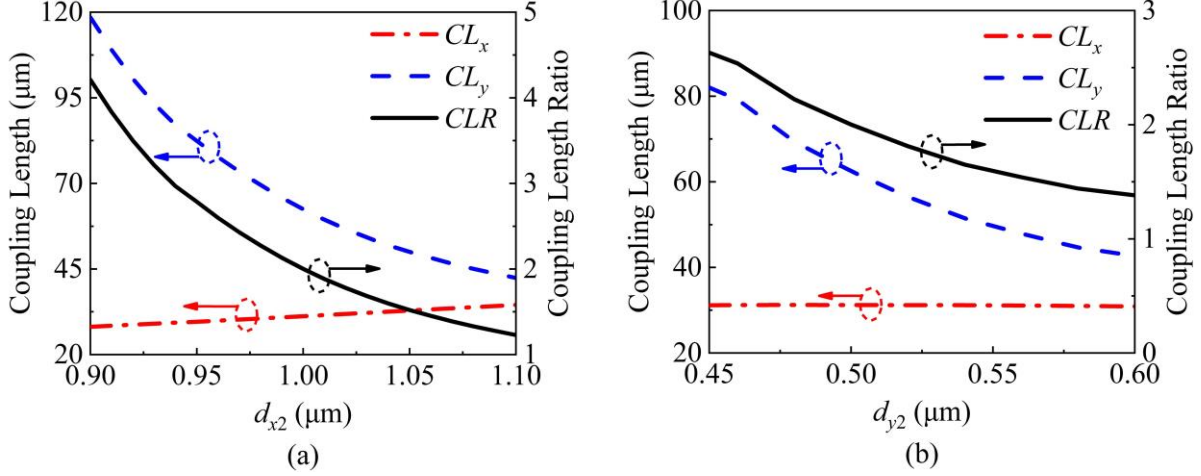


**Fig. 5.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $A_1$  and (b)  $A_2$ .



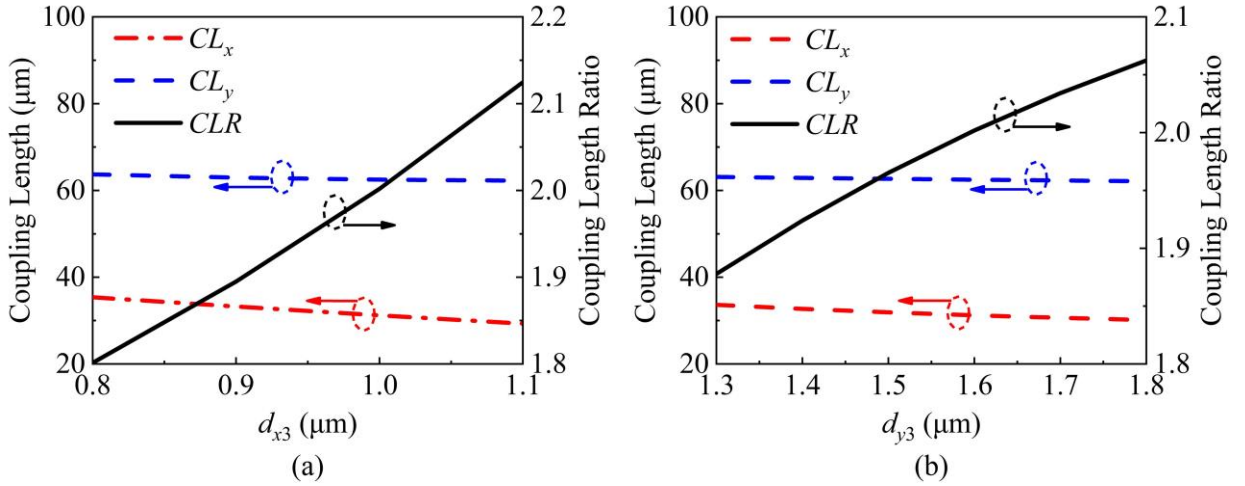
**Fig. 6.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x1}$  and (b)  $d_{y1}$ .

The influences of the elliptical hole sizes are shown in Figs. 6(a) and 6(b). When  $d_{x1}$  changes from 0.4 to 0.8  $\mu\text{m}$ , the effective refractive indices of the  $x$ -pol odd and even modes decrease, but the decrease amplitude of the  $x$ -even mode is larger than that of the  $x$ -odd mode. Although the effective refractive index of the  $y$ -pol odd mode remains almost unchanged, the effective refractive index of the  $y$ -pol even mode gradually decreases. Thus, the effective refractive index difference between the  $x$ -pol odd and even modes becomes smaller, and the effective refractive index difference between the  $y$ -pol odd and even modes becomes larger. As shown in Fig. 6(a), the  $CL_x$  increases from 29 to 33  $\mu\text{m}$ , the  $CL_y$  decreases from 67 to 56  $\mu\text{m}$ , and the corresponding  $CLR$  decreases from 2.2 to 1.6. When  $d_{x1}=0.5$   $\mu\text{m}$ , the  $CLR$  is very close to 2. When  $d_{y1}$  increases from 0.6 to 1.2, the effective refractive index difference of the  $x$ -pol odd and even modes becomes smaller, and the effective refractive index difference between the  $y$ -pol odd and even modes also becomes larger. As shown in Fig. 6(b), the  $CL_x$  increases from 25 to 34  $\mu\text{m}$ , the  $CL_y$  decreases from 68 to 62  $\mu\text{m}$ , and the corresponding  $CLR$  decreases from 2.7 to 1.8. When  $d_{y1}=1$   $\mu\text{m}$ , the  $CLR$  is very close to 2.



**Fig. 7.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x2}$  and (b)  $d_{y2}$ .

The influences of the elliptical gold wires are shown in Figs. 7(a) and 7(b). When  $d_{x2}$  changes from 0.9 to 1.1  $\mu\text{m}$ , the effective refractive index of the  $x$ -pol odd mode remains almost unchanged, but the effective refractive index of the  $x$ -pol even mode gradually decreases. Although the effective refractive indices of the  $y$ -pol odd and  $y$ -pol even modes decrease, the decrease amplitude of the  $y$ -pol even mode is larger than that of the  $y$ -pol odd mode. Thus, the effective refractive index difference between the  $x$ -pol odd and  $x$ -pol even modes becomes smaller, and the effective refractive index difference between the  $y$ -pol odd and  $y$ -pol even modes becomes larger. As shown in Fig. 7(a), the  $CL_x$  increases from 28 to 34  $\mu\text{m}$ , the  $CL_y$  decreases from 118 to 42  $\mu\text{m}$ , and the corresponding  $CLR$  decreases from 4.2 to 1.2. When  $d_{x2}=1$   $\mu\text{m}$ , the  $CLR=2$ . When  $d_{y2}$  increases from 0.45 to 0.6, the effective refractive index difference between the  $x$ -pol odd and  $x$ -pol even modes remains almost unchanged, and the effective refractive index difference between the  $y$ -pol odd and  $y$ -pol even modes becomes larger. As shown in Fig. 7(b), the  $CL_x$  is stabilized at 30  $\mu\text{m}$ , the  $CL_y$  decreases from 131 to 42  $\mu\text{m}$ , and the corresponding  $CLR$  decreases from 4.2 to 1.38. When  $d_{y2}=0.5$   $\mu\text{m}$ , the  $CLR$  is very close to 2.



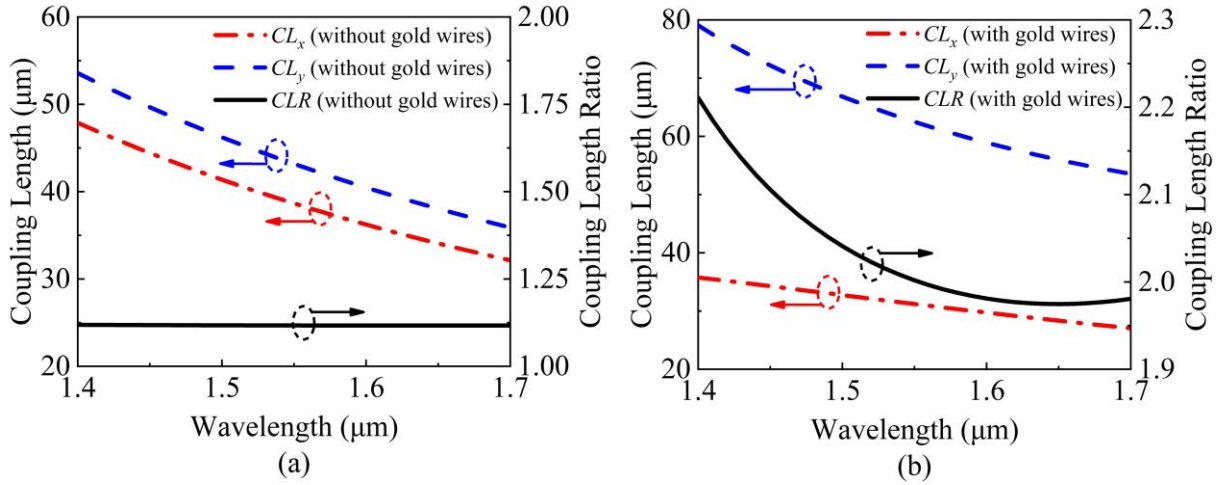
**Fig. 8.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x3}$  and (b)  $d_{y3}$ .

The influences of the large elliptical air hole along the horizontal axis are shown in Figs. 8(a) and 8(b). When  $d_{x3}$  changes from 0.8 to 1.1  $\mu\text{m}$ , the effective refractive index of the  $x$ -pol odd



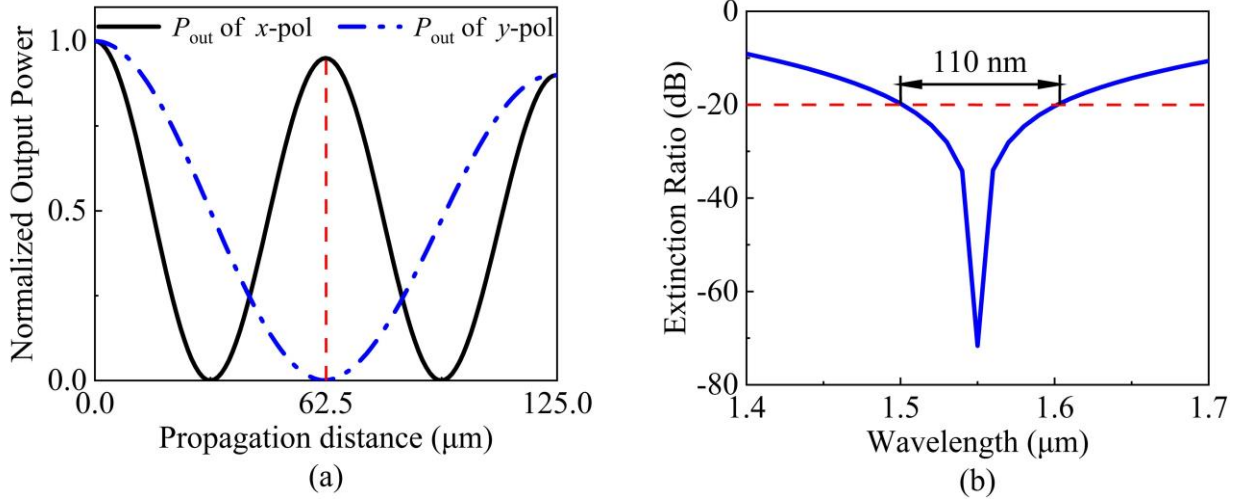
mode decreases slightly, and the effective refractive index of the  $x$ -pol even mode remains almost unchanged. Meanwhile, the effective refractive indices of the  $y$ -pol odd and  $y$ -pol even modes remain almost unchanged. Thus, the effective refractive index difference between the  $x$ -pol odd and  $x$ -pol even modes becomes larger, and the effective refractive index differences between the  $y$ -pol odd and  $y$ -pol even modes changes slightly. From Fig. 8(a), as the  $CL_x$  decreases, the  $CL_y$  is almost constant, and the corresponding  $CLR$  increases. As  $d_{y3}$  increases from 1.3 to 1.8, the effective refractive indices of the  $x$ -pol odd and  $x$ -pol even modes and  $y$ -pol odd and  $y$ -pol even modes decrease, and the decrease amplitudes of the  $x$ -pol odd and  $y$ -pol odd modes are approximately equal to those of the  $x$ -pol even and  $y$ -pol even modes. It can be seen from Fig. 8(b) that the  $CL_x$  and  $CL_y$  are almost constant, but the corresponding  $CLR$  increases.

As shown in Fig. 9(a), when the gold wire is not filled in the two elliptical air holes, the  $CLR$  can only maintain at 1.1 in the wavelength range from 1.4 to 1.7  $\mu\text{m}$ . At this time, it is difficult to completely split the polarized light between the two cores. As shown in Fig. 9(b), when the two elliptical air holes are filled with the gold wires, the  $CLR$  decreases from 2.21 to 1.98 in the considered wavelength range, and reaches 2 at wavelength 1.55  $\mu\text{m}$ . Therefore, the gold wire plays an important role in achieving the PBS.



**Fig. 9.** The relationships between the  $CL$  and  $CLR$  and wavelength, (a) without gold wires, and (b) with gold wires.

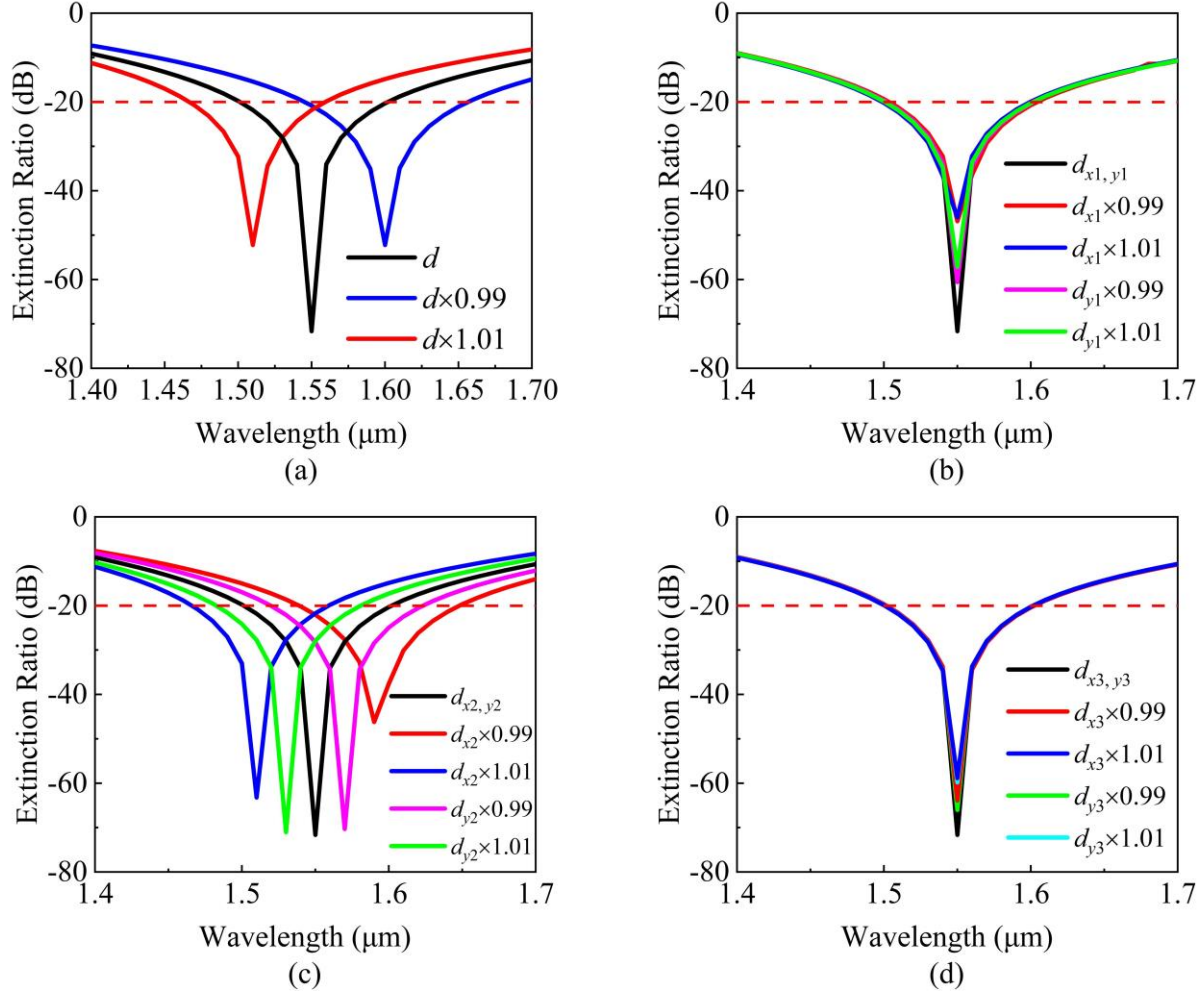
In summary, the optimized structure parameters of the DC-PCF PBS are chosen as following:  $A_1=1.11 \mu\text{m}$ ,  $A_2=1.5 \mu\text{m}$ ,  $d=1 \mu\text{m}$ ,  $d_{x1}=0.5 \mu\text{m}$ ,  $d_{y1}=1 \mu\text{m}$ ,  $d_{x2}=1 \mu\text{m}$ ,  $d_{y2}=0.5 \mu\text{m}$ ,  $d_{x3}=1 \mu\text{m}$ , and  $d_{y3}=1.6 \mu\text{m}$ . Fig. 10(a) shows the relationship between  $P_{\text{out}}$  of  $x$ -pol and  $y$ -pol and propagation distance. As shown in Fig. 10(a), when the light at wavelength 1.55  $\mu\text{m}$  enters the core A,  $P_{\text{out}}$  of the  $x$ -pol and  $y$ -pol will periodically change with the propagation distance. When the propagation distance is 62.5  $\mu\text{m}$ ,  $P_{\text{out}}$  of the  $x$ -pol reaches the maximum value, and  $P_{\text{out}}$  of the  $y$ -pol is close to 0. At this time, the two polarization states can be completely separated. For the core B, the case is exactly opposite. Due to the ohmic loss of metal, the maximum value of the normalized power will decrease with the propagation distance 36. Thus, the optimal DC-PCF PBS length is 62.5  $\mu\text{m}$ . Fig. 10(b) shows the relationship between the  $ER$  and wavelength when the DC-PCF PBS length is 62.5  $\mu\text{m}$ . It can be seen from Fig. 10(b) that the  $ER$  reaches the maximum value of -71 dB at wavelength 1.55  $\mu\text{m}$ , and is less than -20 dB in the wavelength range of 1.5 to 1.61  $\mu\text{m}$ . The bandwidth of the DC-PCF PBS is 110 nm, covering the whole C band.



**Fig. 10.** (a) The relationship between  $P_{\text{out}}$  of the x-pol and y-pol and propagation distance, and (b) the relationship between the  $ER$  and wavelength.

Table 1. The comparisons between other proposed PCF PBSs and this work.

Reference	PBS length	Bandwidth	$ER$ at 1550 nm
22	1.890 mm	9 nm	-83.2 dB
23	0.175 mm	250 nm	-80.7 dB
25	1.0 mm	280 nm	-83.6 dB
26	1.746 mm	47 nm	-60 dB
<b>Error! Reference source not found.</b>	830 μm	20 nm	-60 dB
[42]	254.6 μm	560 nm	-111 dB
This work	62.5 μm	110 nm	-71 dB



**Fig. 11.** The relationships between the *ER* and wavelength under  $\pm 1\%$  error of (a)  $d$ , (b)  $d_{x1}$ ,  $d_{y1}$  (c)  $d_{x2}$ ,  $d_{y2}$ , and (d)  $d_{x3}$ ,  $d_{y3}$ .

Table 1 shows the comparisons between other proposed PCF PBSs and this work [37-42]. It can be concluded from Table 1 that although the bandwidths of the PBSs proposed in Refs [38, 39, 42] are slightly wider than that of this work, the DC-PCF PBS proposed in this work has the shortest length. This is more conducive to the development of photonic integration. Moreover, the bandwidth and *ER* are also good. Finally, we will consider the fabrication tolerance of the proposed DC-PCF PBS. We investigated the dependence of the *ER* on each structure parameter under the fabrication tolerance of 1%. As shown in Fig. 11(a), when  $d$  is reduced or increased by 1%, the bandwidth is red-shifted to 1.54 - 1.64  $\mu\text{m}$  or blue-shifted to 1.46 - 1.56  $\mu\text{m}$ . The DC-PCF PBS can still work well. As shown in Figs. 11(b) and 11(d), when  $d_{x1}$  and  $d_{y1}$ , and  $d_{x3}$  and  $d_{y3}$  are reduced or increased by 1%, only the *ER* at wavelength 1.55  $\mu\text{m}$  is changed, and the bandwidth of the proposed DC-PCF PBS does not change. As shown in Fig. 11(c), when  $d_{x2}$  and  $d_{y2}$  are reduced by 1%, the bandwidth is blue-shifted to 1.53 - 1.65  $\mu\text{m}$  and 1.51 - 1.63  $\mu\text{m}$ , respectively. When  $d_{x2}$  and  $d_{y2}$  are increased by 1%, the bandwidth is red-shifted to 1.43- 1.57  $\mu\text{m}$  and 1.41- 1.57  $\mu\text{m}$ , respectively. Therefore, the proposed DC-PCF PBS has good fabrication tolerance.

#### 4. Conclusion

In conclusion, we design an ultra-short DC-PCF PBS based on the SPR effect. The performance of the proposed DC-PCF PBS is optimized through adjusting structure parameters. The  $CLR$  at wavelength  $1.55\ \mu\text{m}$  is very close to 2. The optimized DC-PCF PBS length is  $62.5\ \mu\text{m}$ , the  $ER$  at wavelength  $1.55\ \mu\text{m}$  is  $-68.76\ \text{dB}$ , and the bandwidth is  $110\ \text{nm}$  ( $1.5 - 1.61\ \mu\text{m}$ ), which can cover the whole C band. The proposed DC-PCF PBS has ultra-short length, large bandwidth, and high  $ER$ , and can find important application in the micro-optical system.

#### Disclosures

The authors declare no conflicts of interest.

#### Acknowledgement

This work is supported by National Key Research and Development Project of China (2019YFB2204001).

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## Captions List

**Fig. 1.** The cross-section of the proposed DC-PCF PBS.

**Fig. 2.** The effective refractive indices of the  $x$ -pol odd and even modes,  $y$ -pol odd and even modes,  $x$ -pol and  $y$ -pol first SPP modes, and zero SPP mode calculated as functions of wavelength.

**Fig. 3.** The mode field distributions of the  $x$ -pol odd mode,  $x$ -pol even mode,  $y$ -pol odd mode, and  $y$ -pol even mode calculated at wavelengths (a)  $1.05\ \mu\text{m}$  and (b)  $1.55\ \mu\text{m}$ .

**Fig. 4.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and  $d$ .

**Fig. 5.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $A_1$  and (b)  $A_2$ .

**Fig. 6.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x1}$  and (b)  $d_{y1}$ .

**Fig. 7.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x2}$  and (b)  $d_{y2}$ .

**Fig. 8.** The relationships between the  $CL_x$ ,  $CL_y$ , and  $CLR$  and (a)  $d_{x3}$  and (b)  $d_{y3}$ .

**Fig. 9.** The relationships between the  $CL$  and  $CLR$  and wavelength, (a) without gold wires, and (b) with gold wires.

405 **Fig. 10.** The relationship between  $P_{\text{out}}$  of the  $x$ -pol and  $y$ -pol and propagation distance, and (b)  
406 the relationship between the  $ER$  and wavelength.

407 **Fig. 11.** The relationships between the  $ER$  and wavelength under  $\pm 1\%$  error of (a)  $d$ , (b)  $dx_1$ ,  $dy_1$   
408 (c)  $dx_2$ ,  $dy_2$ , and (d)  $dx_3$ ,  $dy_3$ .

409 **Table 1.** The comparisons between other proposed PCF PBS and this work.